LM148/LM248/LM348
Quad 741 Op Amps

LM149
Wide Band Decompenesated \((A_V (\text{MIN}) = 5)\)

General Description
The LM148 series is a true quad 741. It consists of four independent, high gain, internally compensated, low power operational amplifiers which have been designed to provide functional characteristics identical to those of the familiar 741 operational amplifier. In addition the total supply current for all four amplifiers is comparable to the supply current of a single 741 type op amp. Other features include input offset currents and input bias current which are much less than those of a standard 741. Also, excellent isolation between amplifiers has been achieved by independently biasing each amplifier and using layout techniques which minimize thermal coupling. The LM149 series has the same features as the LM148 plus a gain bandwidth product of 4 MHz at a gain of 5 or greater.

The LM148 can be used anywhere multiple 741 or 1558 type amplifiers are being used and in applications where amplifier matching or high packing density is required. For lower power refer to LF444.

Features
- 741 op amp operating characteristics
- Class AB output stage — no crossover distortion
- Pin compatible with the LM124
- Overload protection for inputs and outputs
- Low supply current drain: 0.6 mA/Amplifier
- Low input offset voltage: 1 mV
- Low input offset current: 4 nA
- Low input bias current: 30 nA
- High degree of isolation between amplifiers: 120 dB
- Gain bandwidth product
  - LM148 (unity gain): 1.0 MHz
  - LM149 (\(A_V \geq 5\)): 4 MHz

Schematic Diagram

* 1 pF in the LM149
**Absolute Maximum Ratings** *(Note 4)*

If Military/Aerospace specified devices are required, please contact the National Semiconductor Sales Office/Distributors for availability and specifications.

<table>
<thead>
<tr>
<th>Parameter</th>
<th>LM148/LM149</th>
<th>LM248</th>
<th>LM348</th>
</tr>
</thead>
<tbody>
<tr>
<td>Supply Voltage</td>
<td>±22V</td>
<td>±18V</td>
<td>±18V</td>
</tr>
<tr>
<td>Differential Input Voltage</td>
<td>±44V</td>
<td>±36V</td>
<td>±36V</td>
</tr>
<tr>
<td>Output Short Circuit Duration</td>
<td>Continuous</td>
<td>Continuous</td>
<td>Continuous</td>
</tr>
<tr>
<td>Power Dissipation <em>(Pd at 25°C)</em></td>
<td>Continuous</td>
<td>Continuous</td>
<td>Continuous</td>
</tr>
<tr>
<td>Thermal Resistance (θja)</td>
<td>—</td>
<td>—</td>
<td>750 mW</td>
</tr>
<tr>
<td>Molded DIP (N) <em>(Pd)</em></td>
<td>—</td>
<td>—</td>
<td>100˚C/W</td>
</tr>
<tr>
<td>Cavity DIP (J) <em>(Pd)</em></td>
<td>1100 mW</td>
<td>800 mW</td>
<td>700 mW</td>
</tr>
<tr>
<td>Maximum Junction Temperature <em>(TjMAX)</em></td>
<td>150˚C</td>
<td>110˚C</td>
<td>100˚C</td>
</tr>
<tr>
<td>Operating Temperature Range</td>
<td>−55˚C ≤ TA ≤ +125˚C</td>
<td>−25˚C ≤ TA ≤ +85˚C</td>
<td>0˚C ≤ TA ≤ +70˚C</td>
</tr>
<tr>
<td>Storage Temperature Range</td>
<td>−65˚C to +150˚C</td>
<td>−65˚C to +150˚C</td>
<td>−65˚C to +150˚C</td>
</tr>
<tr>
<td>Lead Temperature (Soldering, 10 sec.) Ceramic</td>
<td>300˚C</td>
<td>300˚C</td>
<td></td>
</tr>
<tr>
<td>Lead Temperature (Soldering, 10 sec.) Plastic</td>
<td>260˚C</td>
<td></td>
<td></td>
</tr>
</tbody>
</table>

**Soldering Information**

- Dual-In-Line Package Soldering (10 seconds) 260˚C
- Small Outline Package
  - Vapor Phase (60 seconds) 215˚C
  - Infrared (15 seconds) 220˚C
- See AN-450 “Surface Mounting Methods and Their Effect on Product Reliability” for other methods of soldering surface mount devices.

**ESD tolerance** *(Note 5)*

- 500V

**Electrical Characteristics** *(Note 3)*

<table>
<thead>
<tr>
<th>Parameter</th>
<th>Conditions</th>
<th>LM148/LM149</th>
<th>LM248</th>
<th>LM348</th>
</tr>
</thead>
<tbody>
<tr>
<td>Input Offset Voltage</td>
<td>TA = 25˚C, RB ≤ 10 kΩ</td>
<td>1.0</td>
<td>5.0</td>
<td>1.0</td>
</tr>
<tr>
<td>Input Offset Current</td>
<td>TA = 25˚C</td>
<td>4</td>
<td>25</td>
<td>4</td>
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<tr>
<td>Input Bias Current</td>
<td>TA = 25˚C</td>
<td>30</td>
<td>100</td>
<td>30</td>
</tr>
<tr>
<td>Input Resistance</td>
<td>TA = 25˚C</td>
<td>0.8</td>
<td>2.5</td>
<td>0.8</td>
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<tr>
<td>Supply Current All Amplifiers</td>
<td>TA = 25˚C, VS = ±15V</td>
<td>2.4</td>
<td>3.6</td>
<td>2.4</td>
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<tr>
<td>Large Signal Voltage Gain</td>
<td>TA = 25˚C, VS = ±15V</td>
<td>50</td>
<td>160</td>
<td>25</td>
</tr>
<tr>
<td>Amplifier to Amplifier Coupling</td>
<td>TA = 25˚C, f = 1 Hz to 20 kHz (Input Referred) See Crosstalk Test Circuit</td>
<td>−120</td>
<td>−120</td>
<td>−120</td>
</tr>
<tr>
<td>Small Signal Bandwidth</td>
<td>LM148 Series TA = 25˚C</td>
<td>1.0</td>
<td>1.0</td>
<td>1.0</td>
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<tr>
<td>Phase Margin</td>
<td>LM148 Series TA = 25˚C</td>
<td>60</td>
<td>60</td>
<td>60</td>
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<tr>
<td>Slew Rate</td>
<td>LM148 Series TA = 25˚C</td>
<td>0.5</td>
<td>0.5</td>
<td>0.5</td>
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<tr>
<td>Output Short Circuit Current</td>
<td>TA = 25˚C</td>
<td>25</td>
<td>25</td>
<td>25</td>
</tr>
<tr>
<td>Input Offset Voltage</td>
<td>RB ≤ 10 kΩ</td>
<td>6.0</td>
<td>7.5</td>
<td>7.5</td>
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<tr>
<td>Input Offset Current</td>
<td></td>
<td>75</td>
<td>125</td>
<td>100</td>
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Electrical Characteristics (Continued)

(Note 3)

<table>
<thead>
<tr>
<th>Parameter</th>
<th>Conditions</th>
<th>LM148/LM149</th>
<th>LM248</th>
<th>LM348</th>
<th>Units</th>
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<tbody>
<tr>
<td></td>
<td></td>
<td>Min</td>
<td>Typ</td>
<td>Max</td>
<td>Min</td>
</tr>
<tr>
<td>Input Bias Current</td>
<td>$V_S = \pm 15V$, $V_{OUT} = \pm 10V$, $R_L &gt; 2, \text{k}\Omega$</td>
<td>325</td>
<td>500</td>
<td>400</td>
<td>nA</td>
</tr>
<tr>
<td>Large Signal Voltage Gain</td>
<td>$V_S = \pm 15V$, $V_{OUT} = \pm 10V$, $R_L = 2, \text{k}\Omega$</td>
<td>25</td>
<td>15</td>
<td>15</td>
<td>V/mV</td>
</tr>
<tr>
<td>Output Voltage Swing</td>
<td>$V_S = \pm 15V$, $R_L = 10, \text{k}\Omega$</td>
<td>70</td>
<td>90</td>
<td>70</td>
<td>V</td>
</tr>
<tr>
<td>Common-Mode Rejection Ratio</td>
<td>$R_{IS} \leq 10, \text{k}\Omega$, $\pm 12\leq V_S \leq \pm 15V$</td>
<td>77</td>
<td>96</td>
<td>77</td>
<td>dB</td>
</tr>
<tr>
<td>Supply Voltage Rejection Ratio</td>
<td>$R_{IS} \leq 10, \text{k}\Omega$, $\pm 5\leq V_S \leq \pm 15V$</td>
<td>77</td>
<td>96</td>
<td>77</td>
<td>dB</td>
</tr>
</tbody>
</table>

Note 1: Any of the amplifier outputs can be shorted to ground indefinitely; however, more than one should not be simultaneously shorted as the maximum junction temperature will be exceeded.

Note 2: The maximum power dissipation for these devices must be derated at elevated temperatures and is dictated by $P_d = (T_{JMAX} - T_A)/\theta_{JA}$ or the 25°C $P_{dMAX}$, whichever is less.

Note 3: These specifications apply for $V_S = \pm 15V$ and over the absolute maximum operating temperature range ($T_L \leq T_A \leq T_H$) unless otherwise noted.

Note 4: Refer to RETS 148X for LM148 military specifications and refer to RETS 149X for LM149 military specifications.

Note 5: Human body model, 1.5 k\Omega in series with 100 pF.

Cross Talk Test Circuit

Application Hints

The LM148 series are quad low power 741 op amps. In the proliferation of quad op amps, these are the first to offer the convenience of familiar, easy to use operating characteristics of the 741 op amp. In those applications where 741 op amps have been employed, the LM148 series op amps can be employed directly with no change in circuit performance.

The LM149 series has the same characteristics as the LM148 except it has been decompensated to provide a wider bandwidth. As a result the part requires a minimum gain of 5.
Typical Performance Characteristics

Supply Current

Supply Voltage (V) vs. Supply Current (mA)

Input Bias Current

Temperature (°C) vs. Input Bias Current (mA)

Voltage Swing

Peak to Peak Output Swing (V) vs. Supply Voltage (V)

Positive Current Limit

Output Source Current (mA) vs. Positive Output Voltage Swing (V)

Negative Current Limit

Output Sink Current (mA) vs. Negative Output Voltage Swing (V)

Output Impedance

Frequency (Hz) vs. Output Impedance (Ω)

Common-Mode Rejection Ratio

Frequency (Hz) vs. CMRR (dB)

Open Loop Frequency Response

Gain (dB) vs. Frequency (Hz)

Bode Plot LM148

Frequency (Hz) vs. Gain (dB)

Frequency (MHz) vs. Phase Margin
Typical Performance Characteristics (Continued)

Bode Plot LM149

Large Signal Pulse Response (LM148)

Large Signal Pulse Response (LM149)

Small Signal Pulse Response (LM148)

Small Signal Pulse Response (LM149)

Undistorted Output Voltage Swing

Gain Bandwidth

Slew Rate

Inverting Large Signal Pulse Response (LM149)
Typical Performance Characteristics (Continued)

Application Hints

The LM148 series are quad low power 741 op amps. In the proliferation of quad op amps, these are the first to offer the convenience of familiar, easy to use operating characteristics of the 741 op amp. In those applications where 741 op amps have been employed, the LM148 series op amps can be employed directly with no change in circuit performance.

The LM149 series has the same characteristics as the LM148 except it has been decompensated to provide a wider bandwidth. As a result the part requires a minimum gain of 5.

The pin-outs are such that the inverting input of each amplifier is adjacent to its output. In addition, the amplifier outputs are located in the corners of the package which simplifies PC board layout and minimizes package related capacitive coupling between amplifiers.

The input characteristics of these amplifiers allow differential input voltages which can exceed the supply voltages. In addition, if either of the input voltages is within the operating common-mode range, the phase of the output remains correct. If the negative limit of the operating common-mode range is exceeded at both inputs, the output voltage will be positive. For input voltages which greatly exceed the maximum supply voltages, either differentially or common-mode, resistors should be placed in series with the inputs to limit the current.

Like the LM741, these amplifiers can easily drive a 100 pF capacitive load throughout the entire dynamic output voltage and current range. However, if very large capacitive loads must be driven by a non-inverting unity gain amplifier, a resistor should be placed between the output (and feedback connection) and the capacitance to reduce the phase shift resulting from the capacitive loading.

The output current of each amplifier in the package is limited. Short circuits from an output to either ground or the power supplies will not destroy the unit. However, if multiple output shorts occur simultaneously, the time duration should be short to prevent the unit from being destroyed as a result of excessive power dissipation in the IC chip.
Application Hints (Continued)

As with most amplifiers, care should be taken lead dress, component placement and supply decoupling in order to ensure stability. For example, resistors from the output to an input should be placed with the body close to the input to minimize “pickup” and maximize the frequency of the feedback pole which capacitance from the input to ground creates.

A feedback pole is created when the feedback around any amplifier is resistive. The parallel resistance and capacitance from the input of the device (usually the inverting input) to AC ground set the frequency of the pole. In many instances the frequency of this pole is much greater than the expected 3 dB frequency of the closed loop gain and consequently there is negligible effect on stability margin. However, if the feedback pole is less than approximately six times the expected 3 dB frequency a lead capacitor should be placed from the output to the input of the op amp. The value of the added capacitor should be such that the RC time constant of this capacitor and the resistance it parallels is greater than or equal to the original feedback pole time constant.

Typical Applications—LM148

One Decade Low Distortion Sinewave Generator

![Circuit Diagram]

\[ f = \frac{1}{2\pi R1C1} \times \sqrt{\frac{R4R5}{R3}} \left( \frac{1}{R4} + \frac{1}{R5} \right) \]

\[ f_{\text{MAX}} = 5 \text{ kHz}, \ THD \leq 0.03\% \]

R1 = 100k pot, C1 = 0.0047 µF, C2 = 0.01 µF, C3 = 0.1 µF, R2 = R6 = R7 = 1M, R3 = 5.1k, R4 = 120, R5 = 240Ω, Q = NS5102, D1 = 1N914, D2 = 3.6V avalanche diode (ex. LM103), V_S = ±15V

A simpler version with some distortion degradation at high frequencies can be made by using A1 as a simple inverting amplifier, and by putting back to back zeners in the feedback loop of A3.
Typical Applications—LM148 (Continued)

Low Cost Instrumentation Amplifier

\[
V_{\text{OUT}} = 2\left(\frac{2R}{R_1} + 1\right), V_S - 3V < V_{\text{IN,CM}} < V_S + 3V,
\]

\(V_S = \pm 15V\)
\(R = R_2\), trim \(R_2\) to boost CMRR

Low Drift Peak Detector with Bias Current Compensation

Adjust \(R\) for minimum drift
\(D_3\) low leakage diode
\(D_1\) added to improve speed
\(V_S = \pm 15V\)

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Typical Applications—LM148 (Continued)

Universal State-Variable Filter

\[ V_{in}(s) = \frac{N_{HP}(s)}{D(s)} \]

\[ V_{in}(s) = \frac{S^2}{D(s)} \]

\[ N_{HP}(s) = S^2 \cdot H_{HP} \]

\[ N_{LP}(s) = -\frac{S \cdot \omega_0 \cdot H_{LP}}{Q} \]

\[ N_{LP}(s) = \omega_0^2 \cdot H_{LP} \]

\[ f_0 = \frac{1}{2\pi} \sqrt{\frac{R_6}{R_5}} \left( \frac{1}{\sqrt{1 + \frac{R_6}{R_5}}} \right) \]

\[ Q = \left( \frac{1 + \frac{R_4}{R_3} + \frac{R_4}{R_0}}{1 + \frac{R_6}{R_5}} \right) \left( \frac{R_6}{R_5} \right)^{1/2} \]

\[ H_{HP} = \frac{1 + R_4}{1 + R_3 + R_4} \]

\[ H_{LP} = \frac{1 + R_5}{1 + R_3 + R_4} \]

Tune Q through R0.

For predictable results: \( f_0 < 4 \times 10^4 \)

Use Band Pass output to tune for Q.
Typical Applications—LM148 (Continued)

A 1 kHz 4 Pole Butterworth

\[
\begin{align*}
V_{IN} &\rightarrow 150k \rightarrow 455.6k \rightarrow 10k \\
&\downarrow \\
&\uparrow \quad 1/4 \text{ LM148} \quad + \\
&\downarrow \\
&\uparrow \quad 1/4 \text{ LM148} \quad + \\
&\downarrow \\
&\uparrow \quad 1/4 \text{ LM148} \quad + \\
&\downarrow \\
&\uparrow \quad 1/4 \text{ LM148} \quad + \\
&\downarrow \\
&\downarrow \\
&\downarrow \\
&\downarrow \\
&\downarrow \\
\end{align*}
\]

Use general equations, and tune each section separately
\[Q_{1\text{st\,SECTION}} = 0.541, \quad Q_{2\text{nd\,SECTION}} = 1.306\]
The response should have 0 dB peaking

A 3 Amplifier Bi-Quad Notch Filter

\[
\begin{align*}
V_{IN}(s) &\rightarrow R8 \rightarrow R7 \\
&\downarrow \\
&\uparrow \quad 1/4 \text{ LM148} \quad + \\
&\downarrow \\
&\uparrow \quad 1/4 \text{ LM148} \quad + \\
&\downarrow \\
&\uparrow \quad 1/4 \text{ LM148} \quad + \\
&\downarrow \\
&\downarrow \\
&\downarrow \\
&\downarrow \\
&\downarrow \\
\end{align*}
\]

\[Q = \sqrt{\frac{R6}{R7}} \cdot \frac{R1}{R3} \cdot \frac{C1}{R2} \]
\[f_0 = \frac{1}{2\pi} \sqrt{\frac{R6}{R7}} \cdot \frac{1}{R2} \cdot \frac{C1}{R3} \]
\[f_{\text{NOTCH}} = \frac{1}{2\pi} \sqrt{\frac{R6}{R3R5R7C1C2}} \]

Necessary condition for notch: \[\frac{1}{R6} - \frac{R1}{R4R7}\]

Ex: \[f_{\text{NOTCH}} = 3 \, \text{kHz}, \quad Q = 5, \quad R1 = 270k, \quad R2 = R3 = 20k, \quad R4 = 27k, \quad R5 = 20k, \quad R6 = R8 = 10k, \quad R7 = 100k, \quad C1 = C2 = 0.001 \, \mu F\]
Better noise performance than the state-space approach.
Typical Applications—LM148 (Continued)

A 4th Order 1 kHz Elliptic Filter (4 Poles, 4 Zeros)

R1C1 = R2C2 = t
R1'C'1 = R2'C'2 = t'

f_C = 1 kHz, f_0 = 2 kHz, f_p = 0.543, f_z = 2.14, Q = 0.841, f'_p = 0.987, f'_z = 4.92, Q' = 4.403, normalized to ripple BW

\[ f = \frac{1}{2\pi R1C1} \times \sqrt{K} = \frac{R4R6}{R3} \left( \frac{1}{r_{DS}} + \frac{1}{R4} \right) \times r_{DS} \approx \frac{R_{ON}}{1 - \frac{V_{GS}}{V_{P}}} \times f_0 \]

Use the BP outputs to tune Q, Q', tune the 2 sections separately

R1 = R2 = 92.6k, R3 = R4 = R5 = 100k, R6 = 10k, R0 = 107.8k, R_L = 100k, R_H = 155.1k
R1' = R2' = 50.9k, R4' = R5' = 100k, R6' = 10k, R0' = 5.76k, R_L' = 100k, R_H' = 248.12k, R_T = 100k. All capacitors are 0.001 µF.

Lowpass Response

Gain (dB)

FREQUENCY (Hz)

Gain (dB)

FREQUENCY (Hz)
Typical Applications—LM149

Minimum Gain to Insure LM149 Stability

\[ A_{CL(s)} = \frac{V_{OUT}}{V_{IN}} = \frac{-4}{1 + \frac{5}{A_{OL(s)}}} = -4 \]

\[ V_{O} \bigg|_{V_{IN} = 0} = \pm 0.5 \times V_{OS} \]

Power BW = 40 kHz
Small Signal BW = G BW/5

The LM149 as a Unity Gain Inverter

\[ A_{CL(s)} = \frac{V_{OUT}}{V_{IN}} = \frac{-1}{1 + \frac{6}{A_{OL(s)}}} = -1 \]

\[ V_{O} \bigg|_{V_{IN} = 0} = \pm 0.5 \times V_{OS} \]

Small Signal BW = G BW/5

Non-inverting-Integrator Bandpass Filter

For stability purposes: R7 = R6/4, 10R6 = R5, C_C = 10C

\[ f_0 = \frac{1}{2\pi} \sqrt{\frac{R_5}{R_6}} \cdot \frac{1}{C \cdot Q} \cdot Q = \frac{R_6}{R_5} \cdot \frac{R_5}{R_6} \cdot \text{Hoop} = \frac{R_6}{R_{IN}} \]

f_{0\text{MAX}}, Q_{\text{MAX}} = 20 kHz, 10

Better Q sensitivity with respect to open loop gain variations than the state variable filter.

R7, C_C added for compensation
Typical Applications—LM149 (Continued)

Active Tone Control with Full Output Swing (No Slew Limiting at 20 kHz)

\[ V_{S} = \pm 15V, \quad V_{OUT(MAX)} = 9.1 \text{ V RMS} \]
\[ f_{MAX} = 20 \text{ kHz}, \quad \text{THD} \leq 1\% \]

Duplicate the above circuit for stereo

\[ f_{L} = \frac{1}{2\pi R2C1}, \quad f_{LB} = \frac{1}{2\pi R1C1} \]
\[ f_{H} = \frac{1}{2\pi R5C3}, \quad f_{HB} = \frac{1}{2\pi (R1 + 2R7) C3} \]

Max Bass Gain = \((R1 + R2)/R1\)
Max Treble Gain = \((R1 + 2R7)/R5\)

as shown: \(f_{L} = 32\text{ Hz}, \quad f_{LB} = 320\text{ Hz}\)
\(f_{H} = 11\text{ kHz}, \quad f_{HB} = 1.1\text{ Hz}\)
Typical Applications—LM149 (Continued)

Triangular Squarewave Generator

\[ f = \frac{K \times V_{IN}}{8V^+ C1R1} \cdot \frac{2V_0}{K} \leq 25V, \ V^+ = V^-, \ V_S = \pm 15V \]

Use LM125 for ±15V supply
The circuit can be used as a low frequency V/F for process control.
Q1, Q3: KE4393, Q2, Q4: P1087E, D1–D4 = 1N914
Typical Simulation

LM148, LM149, LM741 Macromodel for Computer Simulation

For more details, see IEEE Journal of Solid-State Circuits, Vol. SC-9, No. 6, December 1974

Note 6: $o_1 = 112 \times 8 \times 10^{-16}$

Note 7: $o_2 = 144 \times C_2 = 6 \text{ pF}$ for LM149
See NS Package Number J14A, M14A or N14A
LM148J is available per JM38510/11001
Ceramic Dual-In-Line Package (J)
NS Package Number J14A

S.O. Package (M)
Order Number LM348M or LM348MX
NS Package Number M14A
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